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(54) DISPLAY DRIVER CIRCUITS

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(57) **ABSTRACT**

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345/211-212, 214-215, 690, 697; 315/169.3
See application file for complete search history.

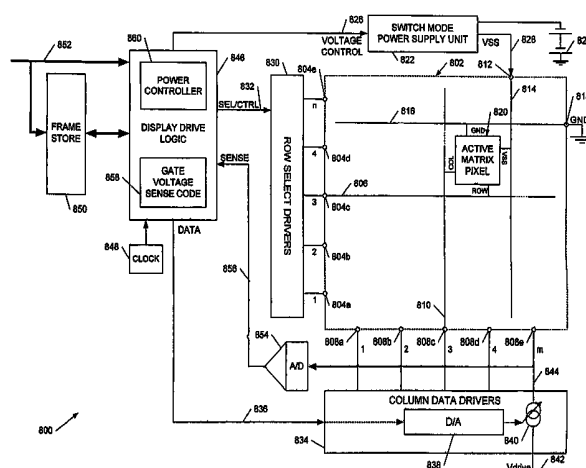
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10 Claims, 10 Drawing Sheets



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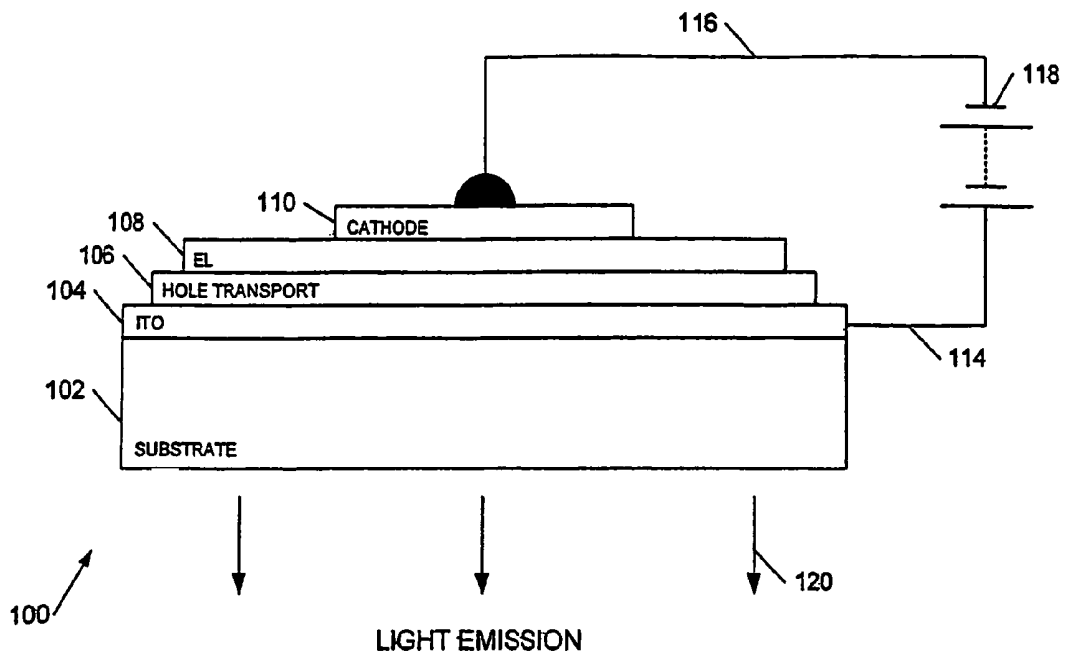


Figure 1a
(PRIOR ART)

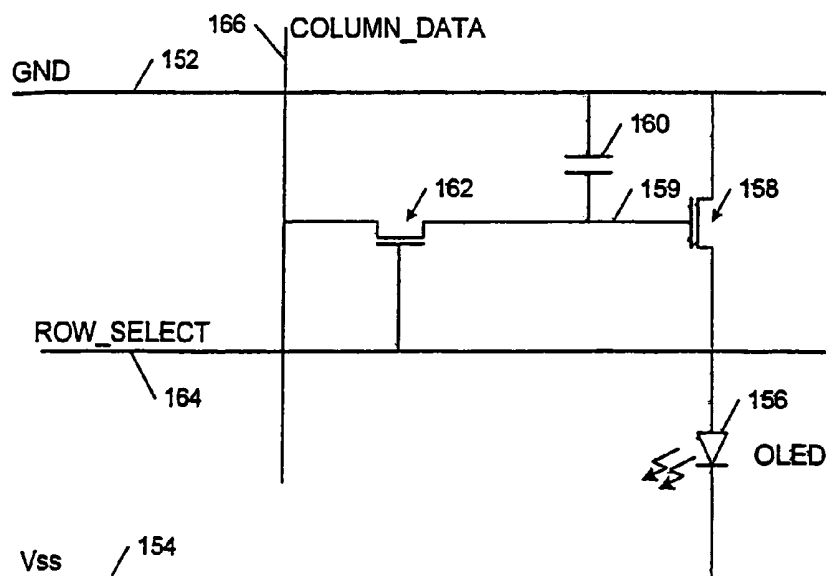


Figure 1b
(PRIOR ART)

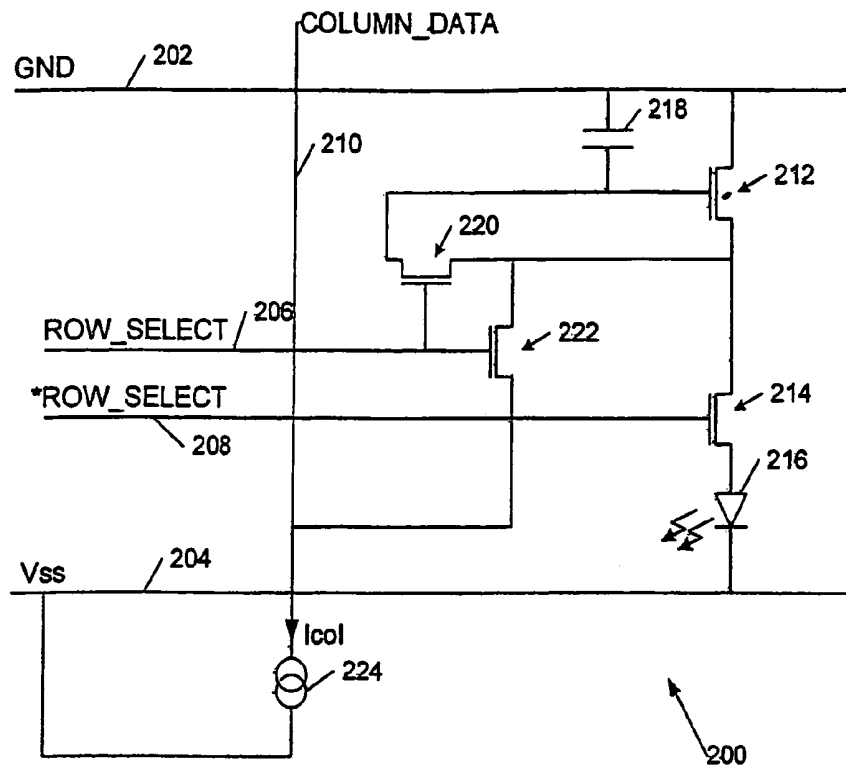


Figure 2a

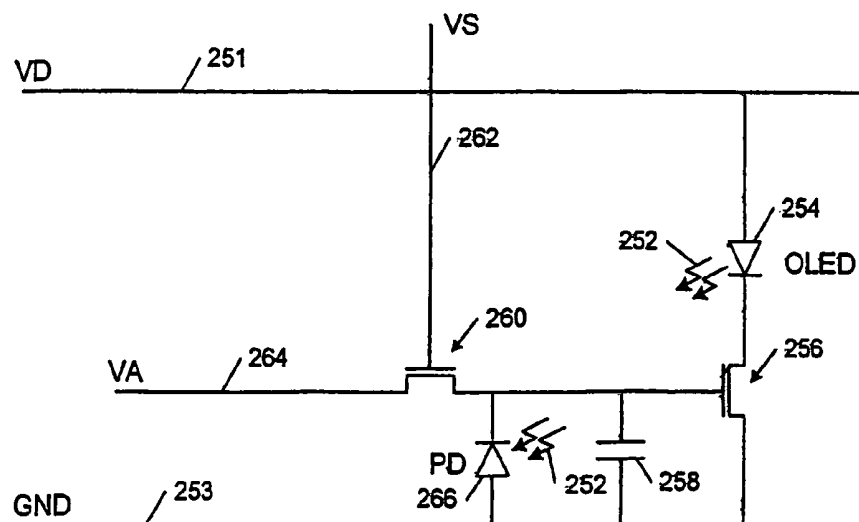


Figure 2b
(PRIOR ART)

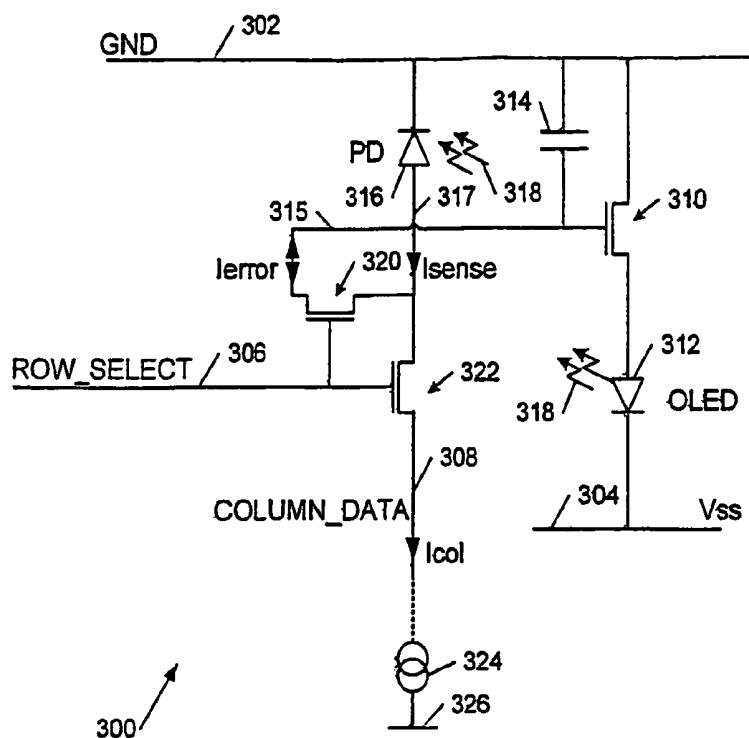


Figure 3a

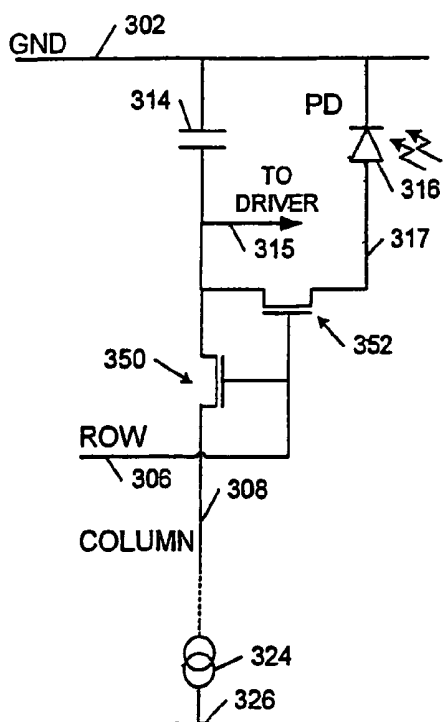


Figure 3b

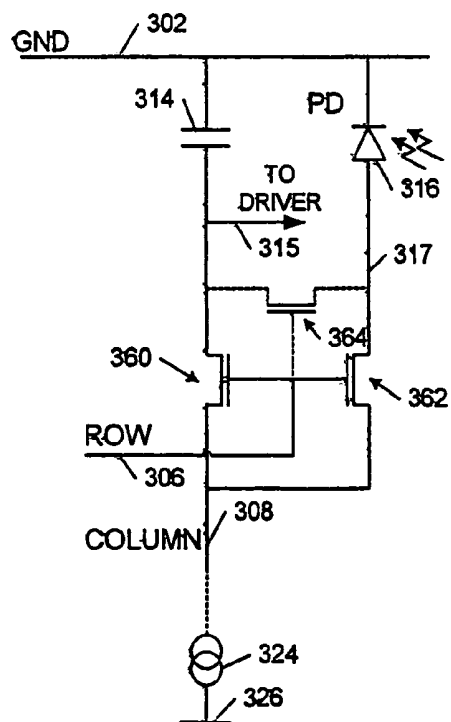


Figure 3c

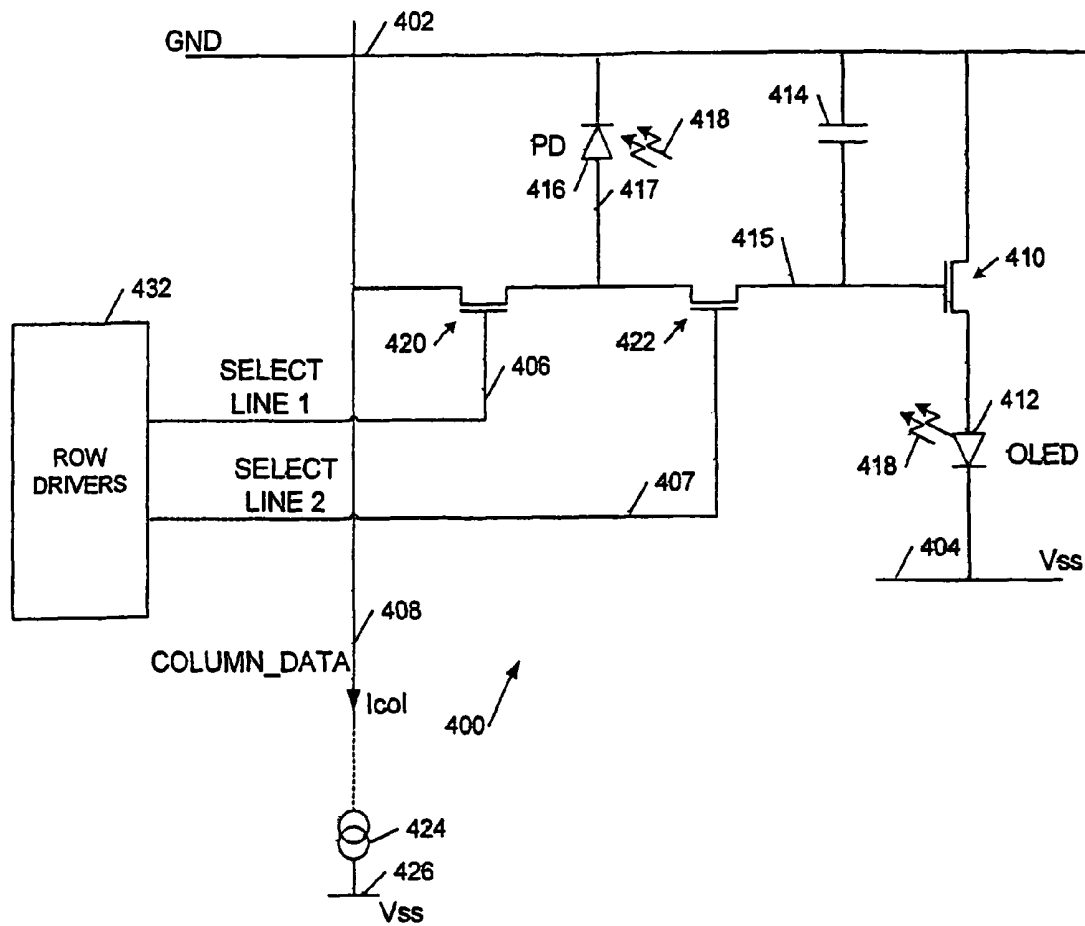


Figure 4

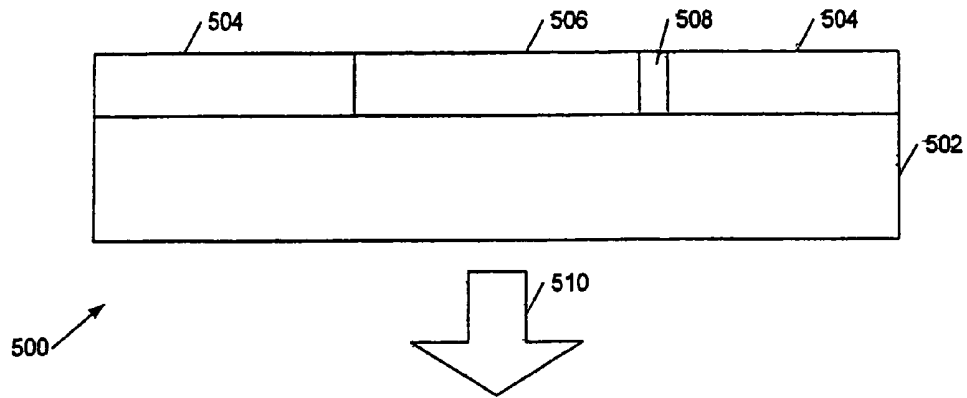


Figure 5a

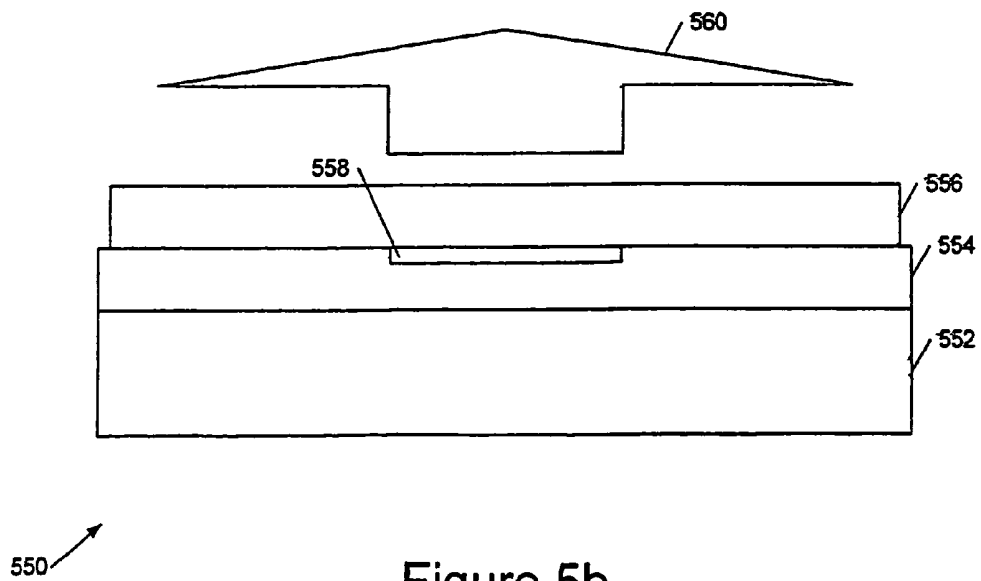


Figure 5b

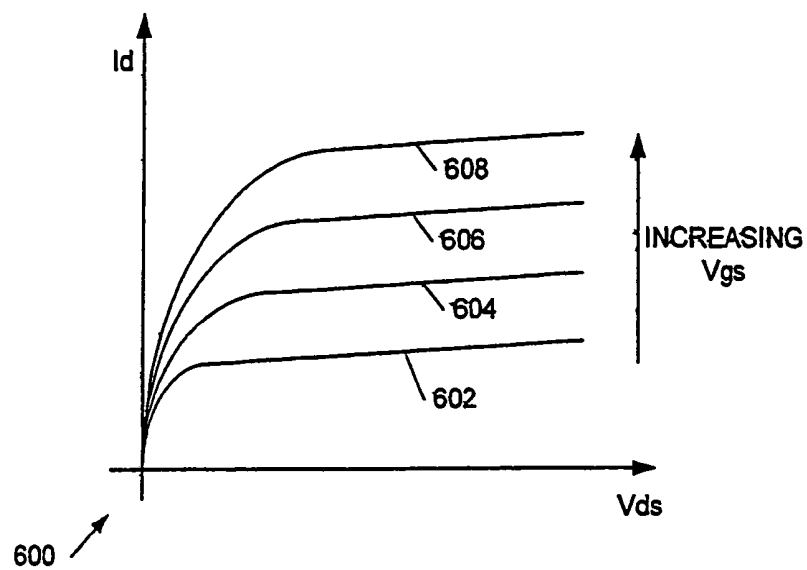


Figure 6a

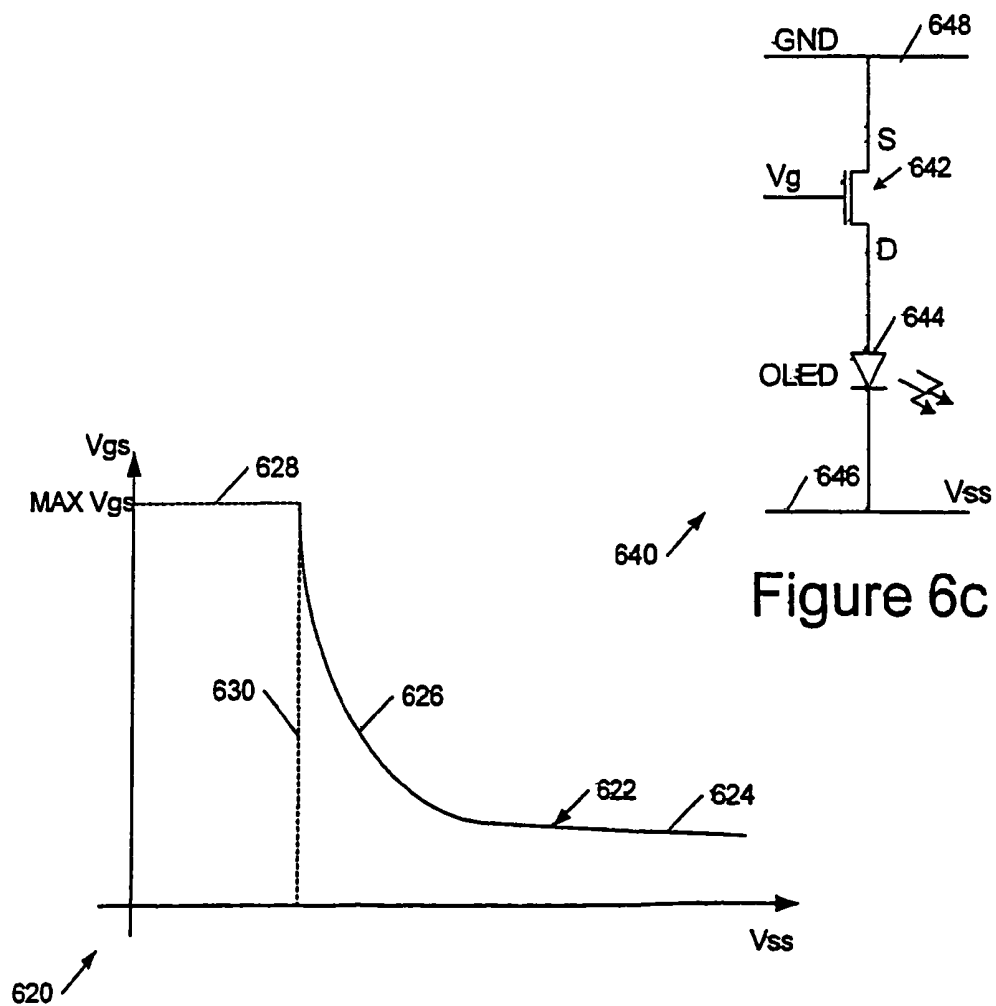


Figure 6c

Figure 6b

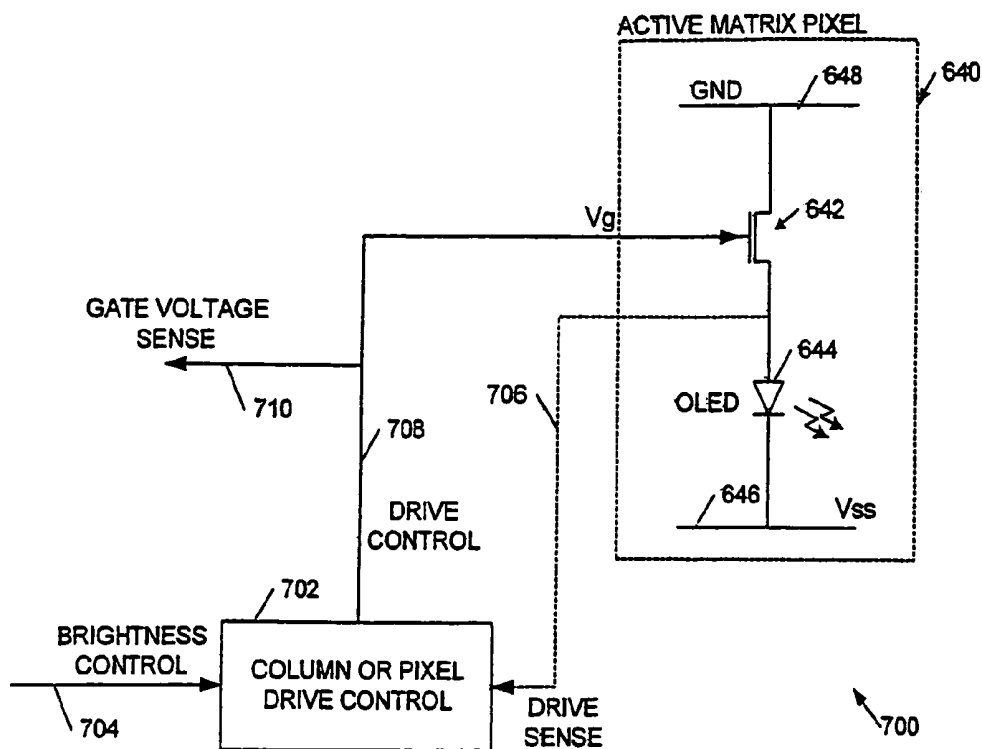


Figure 7a

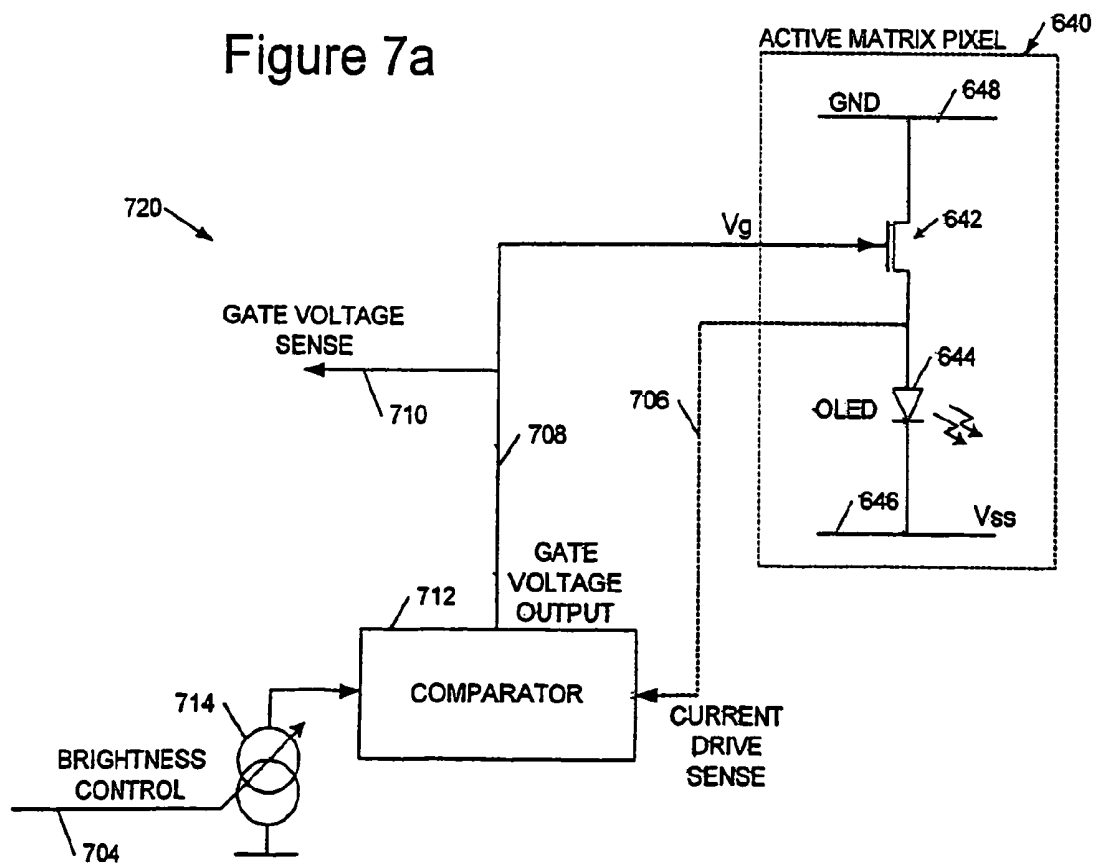


Figure 7b

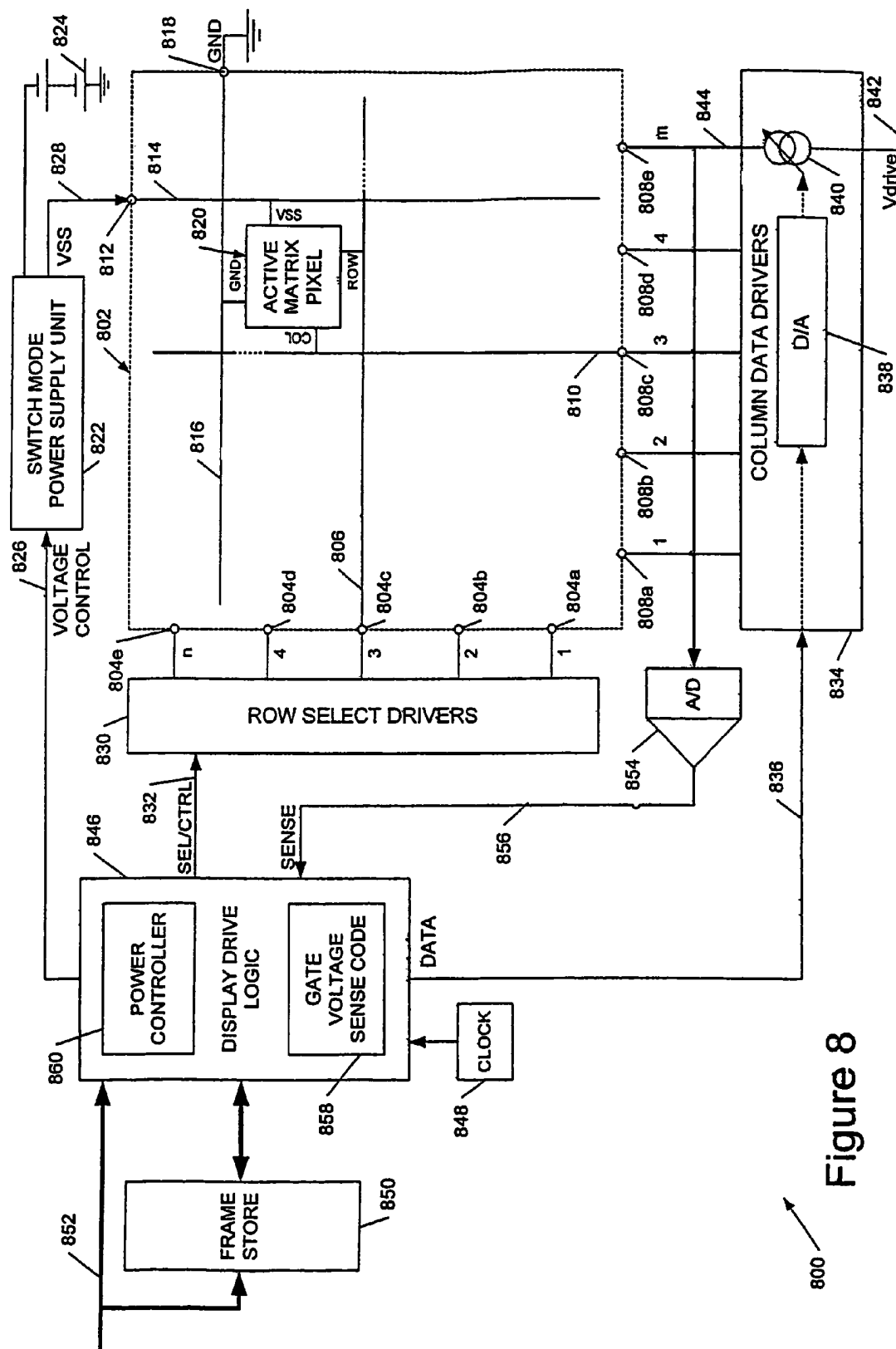


Figure 8

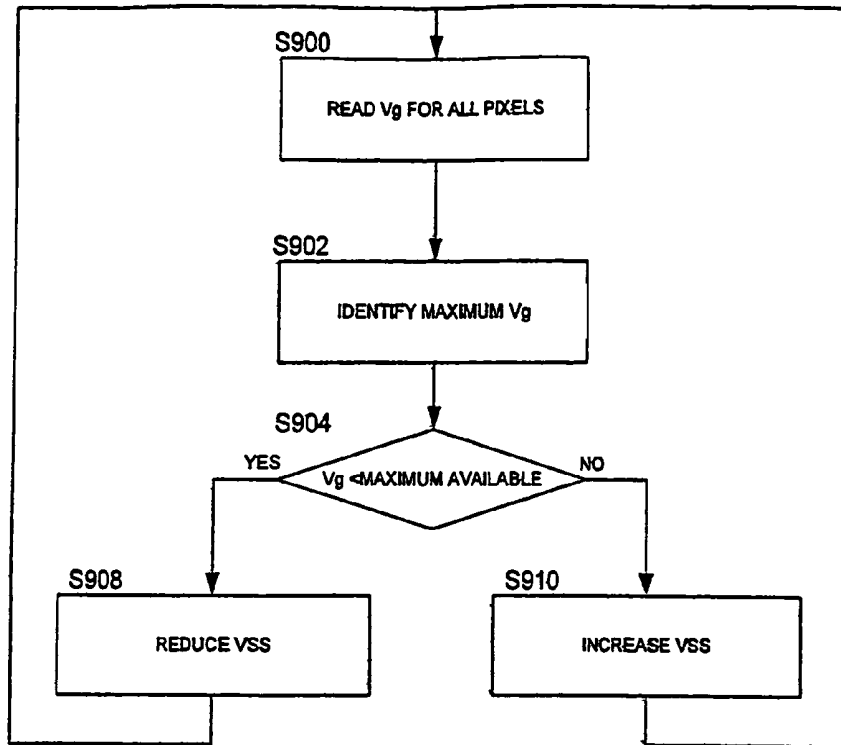


Figure 9a

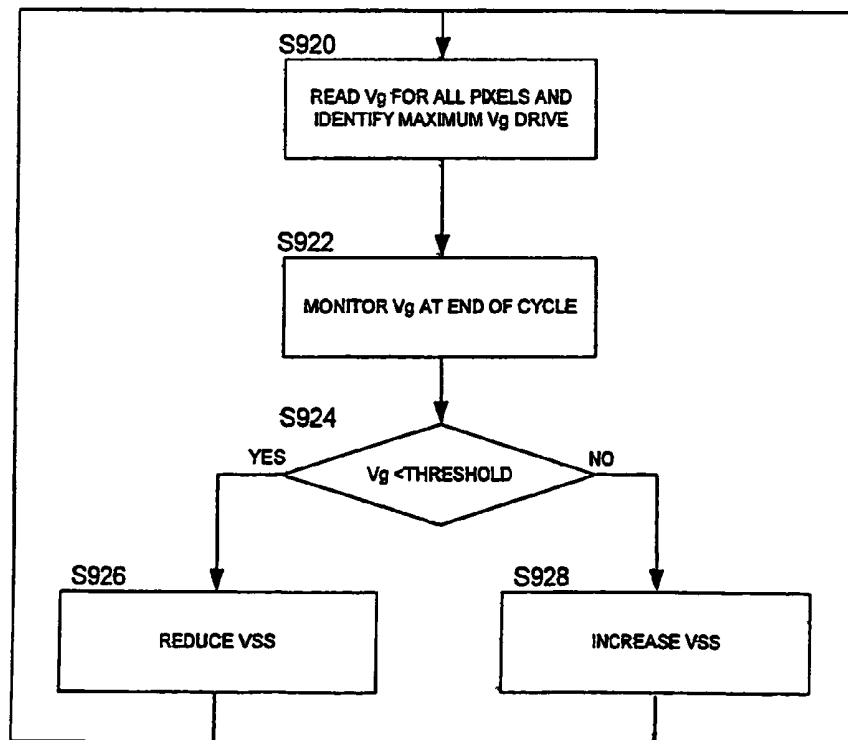


Figure 9b

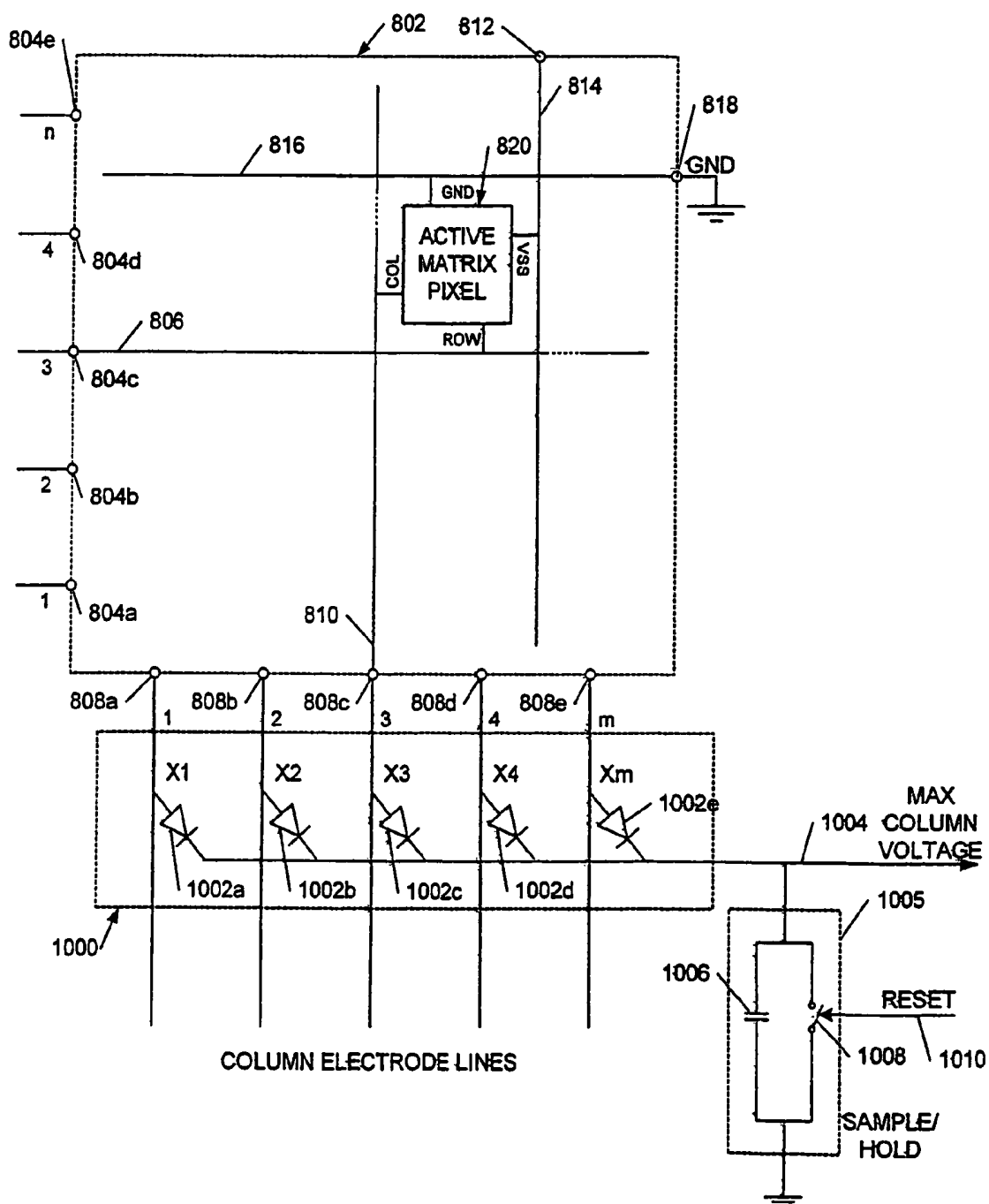


Figure 10

DISPLAY DRIVER CIRCUITS

This is the U.S. national phase of International Application No. PCT/GB03/02529 filed Jun. 11, 2003, the entire disclosure of which is incorporated herein by reference.

This invention generally relates to display driver circuits for electro-optic displays, and more particularly relates to circuits and methods for driving active matrix organic light emitting diode displays with greater efficiency.

Organic light emitting diodes (OLEDs) comprise a particularly advantageous form of electro-optic display. They are bright, colorful fast-switching, provide a wide viewing angle and are easy and cheap to fabricate on a variety of substrates. Organic LEDs may be fabricated using either polymers or small molecules in a range of colours (or in multi-coloured displays), depending upon the materials used. Examples of polymer-based organic LEDs are described in WO 90/13148, WO 95/06400 and WO 99/48160; examples of so called small molecule based devices are described in U.S. Pat. No. 4,539,507.

A basic structure **100** of a typical organic LED is shown in FIG. **1a**. A glass or plastic substrate **102** supports a transparent anode layer **104** comprising, for example, indium tin oxide (ITO) on which is deposited a hole transport layer **106**, an electroluminescent layer **108**, and a cathode **110**. The electroluminescent layer **108** may comprise, for example, a PPV (poly(p-phenylenevinylene)) and the hole transport layer **106**, which helps match the hole energy levels of the anode layer **104** and electroluminescent layer **108**, may comprise, for example, PEDOT:PSS (polystyrene-sulphonate-doped polyethylene-dioxythiophene). Cathode layer **110** typically comprises a low work function metal such as calcium and may include an additional layer immediately adjacent electroluminescent layer **108**, such as a layer of aluminium, for improved electron energy level matching. Contact wires **114** and **116** to the anode the cathode respectively provide a connection to a power source **118**. The same basic structure may also be employed for small molecule devices.

In the example shown in FIG. **1a** light **120** is emitted through transparent anode **104** and substrate **102** and such devices are referred to as "bottom emitters". Devices which emit through the cathode may also be constructed, for example by keeping the thickness of cathode layer **110** less than around 50-100 nm so that the cathode is substantially transparent.

Organic LEDs may be deposited on a substrate in a matrix of pixels to form a single or multi-colour pixellated display. A multicoloured display may be constructed using groups of red, green, and blue emitting pixels. In such displays the individual elements are generally addressed by activating row (or column) lines to select the pixels, and rows (or columns) of pixels are written to, to create a display. It will be appreciated that with such an arrangement it is desirable to have a memory element associated with each pixel so that the data written to a pixel is retained whilst other pixels are addressed. Generally this is achieved by a storage capacitor which stores a voltage set on a gate of a driver transistor. Such devices are referred to as active matrix displays and examples of polymer and small-molecule active matrix display drivers can be found in WO 99/42983 and EP 0,717,446A respectively.

FIG. **1b** shows such a typical OLED driver circuit **150**. A circuit **150** is provided for each pixel of the display and ground **152**, V_{ss} **154**, row select **164** and column data **166** busbars are provided interconnecting the pixels. Thus each pixel has a power and ground connection and each row of

pixels has a common row select line **164** and each column of pixels has a common data line **166**.

Each pixel has an organic LED **156** connected in series with a driver transistor **158** between ground and power lines **152** and **154**. A gate connection **159** of driver transistor **158** is coupled to a storage capacitor **160** and a control transistor **162** couples gate **159** to column data line **166** under control of row select line **164**. Transistor **162** is a field effect transistor (FET) switch which connects column data line **166** to gate **159** and capacitor **160** when row select line **164** is activated. Thus when switch **162** is on a voltage on column data line **166** can be stored on a capacitor **160**. This voltage is retained on the capacitor for at least the frame refresh period because of the relatively high impedances of the gate connection to driver transistor **158** and of switch transistor **162** in its "off" state.

Driver transistor **158** is typically an FET transistor and passes a (drain source) current which is dependent upon the transistor's gate voltage less a threshold voltage. Thus the voltage at gate node **159** controls the current through OLED **156** and hence the brightness of the OLED.

The standard voltage-controlled circuit of FIG. **1b** suffers from a number of drawbacks. The main problems arise because the brightness of OLED **156** is dependent upon the characteristics of the OLED and of the transistor **158** which is driving it. In general, these vary across the area of a display and with time, temperature, and age. This makes it difficult to predict in practice how bright a pixel will appear when driven by a given voltage on column data line **166**. In a colour display the accuracy of colour representations may also be affected.

FIG. **2a** shows a current-controlled pixel driver circuit **200** which addresses these problems. In this circuit the current through an OLED **216** is set by setting a drain source current for OLED driver transistor **212** using a reference current sink **224** and memorising the driver transistor gate voltage required for this drain-source current. Thus the brightness of OLED **216** is determined by the current, I_{cot} , flowing into reference current sink **224**, which is preferably adjustable and set as desired for the pixel being addressed. It will be appreciated that one current sink **224** is provided for each column data line **210** rather than for each pixel.

In more detail, power **202**, **204**, column data **210**, and row select **206** lines are provided as described with reference to the voltage-controlled pixel driver of FIG. **1b**. In addition an inverted row select line **208** is also provided, the inverted row select line being high when row select line **206** is low and vice versa. A driver transistor **212** has a storage capacitor **218** coupled to its gate connection to store a gate voltage for driving the transistor to pass a desired drain-source current. Drive transistor **212** and OLED **216** are connected in series between a power **202** and ground **204** lines and, in addition, a further switching transistor **214** is connected between drive transistor **212** and OLED **216**, transistor **214** having a gate connection coupled to inverted row select line **208**. Two further switching transistors **220**, **222** are controlled by non-inverted row select line **206**.

In the embodiment of the current-controlled pixel driver circuit **200** illustrated in FIG. **2a** all the transistors are PMOS, which is preferable because of their greater stability and better resistance to hot electron effects. However NMOS transistors could also be used.

In the circuit of FIG. **2a** the source connections of the transistors are towards GND and for present generation OLED devices V_{ss} is typically around -6 volts. When the row is active the row select line **206** is thus driven at a more negative voltage, up to approximately -20 volts and inverted row select line **208** is driven at 0 volts.

When row select is active transistors **220** and **222** are turned on and transistor **214** is turned off. Once the circuit has reached a steady state reference current I_{col} into current sink **224** flows through transistor **222** and transistor **212** (the gate of **212** presenting a high impedance). Thus the drain-source current of transistor **212** is substantially equal to the reference current set by current sink **224** and the gate voltage required for this drain-source current is stored on capacitor **218**. Then, when row select becomes inactive, transistors **220** and **222** are turned off and transistor **214** is turned on so that this same current now flows through transistor **212**, transistor **214**, and OLED **216**. Thus the current through OLED is controlled to be substantially the same as that-set by reference current sink **224**.

Before this steady state is reached the voltage on capacitor **218** will generally be different from the required voltage and thus transistor **212** will not pass a drain source current equal to the current, I_{col} , set by reference sink **224**. When such a mismatch exists a current equal to the difference between the reference current and the drain-source current of transistor **212** flows onto or off capacitor **218** through transistor **220** to thereby change the gate voltage of transistor **212**. The gate voltage changes until the drain-source current of transistor **212** equals the reference current set by sink **224**, when the mismatch is eliminated and no current flows through transistor **220**.

In the circuit of FIG. **2a** the maximum (most negative) gate voltage drive is V_{ss} . To permit a greater (more negative) drive voltage reference sink **224** may be connected to a drive voltage V_{drive} more negative than V_{ss} .

The circuit of FIG. **2a** solves some of the problems associated with the voltage-controlled circuit of FIG. **1b** as the current through OLED **216** can be set irrespective of variations in the characteristics of pixel driver transistor **212**. However it is still prone to variations in the characteristics of OLED **216** between pixels, between active matrix display devices, and with temperature and time.

For this reason optical feedback may be employed to control the OLED current, as described in WO 01/20591, EP 0,923,067A, EP 1,096,466A, and JP 5-035,207, which all employ the same basic technique. FIG. **2b**, which is taken from WO 01/20591, illustrates the technique, which is to connect a photodiode across the storage capacitor.

FIG. **2b** shows a voltage-controlled pixel driver circuit **250** with optical feedback **252**. The main components of the driver circuit **250** of FIG. **2b** correspond to those of circuit **150** of FIG. **1b**, that is, an OLED **254** in series with a driver transistor **256** having a storage capacitor **258** coupled to its gate connection. As illustrated, the pixel driver circuit has connections **251** and **253** to, respectively, a positive-supply V_D and to Ground and driver transistor is an NMOS transistor. The skilled person will appreciate that the circuit could also employ a PMOS driver transistor and a negative supply.

A switch transistor **260** is controlled by a row conductor **262** and, when switched on, allows a voltage on capacitor **258** to be set by applying a voltage signal to column conductor **264** or a given charge to be injected into the capacitor. Additionally, however, a photodiode **266** is connected across storage capacitor **258** so that it is reverse biased. Thus photodiode **266** is essentially non-conducting in the dark and exhibits a small reverse conductance depending upon the degree of illumination. The physical structure of the pixel is arranged so that OLED **254** illuminates photodiode **266**, thus providing an optical feedback path **252**.

The photocurrent through photodiode **266** is approximately linearly proportional to the instantaneous light output level from OLED **254**. Thus the charge stored on capacitor

258, and hence the voltage across the capacitor and the brightness of OLED **254**, decays approximately exponentially over time. The integrated light output from OLED **254**, that is the total number of photons emitted and hence the perceived brightness of the OLED pixel, is thus approximately determined by the initial charge stored on capacitor **258**.

Improvements to the circuit of FIG. **2b**, in which every pixel of the display needs refreshing every frame, are described in the applicant's co-pending UK patent applications 0126120.5 and 0126122.1, both filed on 31 Oct. 2001.

FIG. **3a** shows a current-controlled organic LED active matrix pixel driver circuit **300** with optical feedback according to as described in patent application number 0126120.5. In the circuit of FIG. **3a**, and in the circuits described later, the transistors of the active matrix pixels are preferably PMOS.

In an active matrix display typically each pixel is provided with such a pixel driver circuit. Further driver circuitry (not shown in FIG. **3a**) is provided to address the pixels row-by-row, to set each row at the desired brightness. To power and control the pixel driver circuitry and OLED display element such an active matrix display is provided with a grid of electrodes including, as shown in FIG. **3a**, a ground (GND) line **302**, a power or V_{ss} line **304**, a row select line **306** and a column data line **308**. Each column data line is connected to a programmable constant current reference source (or sink) **324**. This is not part of the driver circuitry provided for each pixel but instead comprises part of the display driver circuitry provided for each column. Reference current generator **324** is programmable so that it can be adjusted to a desired level to set a pixel brightness, as described in more detail below.

The pixel driver circuit **300** comprises a driver transistor **310** connected in series with an organic LED display element **312** between the GND **302** and V_{ss} **304** lines. A storage capacitor **314**, which may be integrated with the gate of transistor **310**, stores a charge corresponding to a memorised gate voltage to control the drive-current through OLED element **312**. Control circuitry for the driver comprises two switching transistors **320**, **322** with a common gate connection coupled to row select line **306**. When row select line **306** is active these two switch transistors are on, that is the switches are "closed", and there is a relatively low impedance connection between lines **315**, **317** and **308**. When row select line **306** is inactive transistors **320** and **322** are switched off capacitor **314** and the gate of transistor **310** are effectively isolated, and any voltage set on capacitor **314** is memorised.

A photodiode **316** is coupled between GND line **302** and line **317** so that it is reverse biased. The photodiode is physically arranged with respect to the OLED display element **312** such that an optical feedback path **318** exists between OLED **312** and photodiode **316**. In other words, OLED **312** illuminates photodiode **316** and this allows an illumination-dependent current to flow in a reverse direction through photodiode **316**, that is from GND line **302** towards V_{ss} . As the skilled person will understand, broadly speaking each photon generates an electron within photodiode **316** which can contribute to a photocurrent.

Column data line **308** is coupled, at the end of a column, to programmable reference current generator **324**. This attempts to cause a reference current, which will be referred to as I_{col} , to flow to off-pixel V_{ss} connection **326**. Line **317** may be referred to as a current sense line, passing a current I_{sense} and line **315** may be referred to as a control line, passing a current I_{error} to set a voltage on capacitor **314** to control OLED **312**. When row select line **306** is active and transistors **320** and **322** are on $I_{col} = I_{sense} + I_{error}$, and thus a current I_{error} flows either onto or off capacitor **314** until OLED **312** illuminates photodiode **316** such that $I_{sense} = I_{col}$. At this point row select line

306 can be deactivated, and the voltage required for this level of brightness is memorised by capacitor 314.

Similarly to FIG. 2a, as drawn the maximum (most negative) gate voltage drive for transistor 310 is V_{ss} and to permit a greater (more negative) drive off-pixel connection 326 may be connected to a drive voltage V_{drive} more negative than V_{ss} .

The time required for the voltage on capacitor 314 to stabilise depends upon a number of factors, which may be varied in accordance with the desired device characteristics, and may be a few microseconds. Broadly speaking a typical OLED drive current is of the order of 1 μ A whilst a typical photocurrent is around 0.1% of this, or of the order of 1 nA (in part dependent upon the photodiode area). It can therefore be seen that the power handling requirements of transistors 320 and 322 are negligible compared with that of the drive transistor 310, which must be relatively large. To speed up the settling time of the circuit it is preferable to use a relatively small value for capacitor 314 and a relatively large area photodiode to increase the photocurrent. This also helps reduce the risk of noise and stability at very low brightness levels associated with stray or parasitic capacitance on column data line 308.

FIGS. 3b and 3c show a portion of the circuit of FIG. 3a illustrating different possible configurations for switching transistors corresponding to switching transistors 320 and 322 of FIG. 3a. The purpose of transistors 320 and 322 is to couple lines 315, 317 and 308 when row select line 306 is active and it will be appreciated that there are three different ways of connecting three nodes using two controllable switches.

In FIG. 3b a first switching transistor 350 is connected between lines 308 and 315 and a second switching transistor 352 is connected between lines 315 and 317. Both transistors 350 and 352 are controlled by row select line 306. In FIG. 3c a first switching transistor 360 is connected between lines 308 and 315 and a second switching transistor 362 is connected between lines 308 and 317. Optionally a third switching transistor 364 may be connected between lines 315 and 317. The two (or three) switching transistors are all controlled by row select line 306.

The preferred photosensor is a photodiode which may comprise a PN diode in TFT technology or a PIN diode in crystalline silicon. However other photosensitive devices such as photoresistors and photosensitive bipolar transistors and ETs may also be employed, providing they have a characteristic in which a photocurrent is dependent upon their level of illumination.

The active matrix pixel circuits as described use PMOS transistors but the circuits may be inverted and NMOS employed or, alternatively, a combination of PMOS and NMOS transistors or bipolar transistors may be used. The transistors may comprise thin film transistors (TFTs) fabricated from amorphous or polysilicon on a glass or plastic substrate or conventional CMOS circuitry may be used. Alternatively plastic transistors such as those described in WO 99/54936 may be employed, and the photodiode may comprise a reverse biased OLED to allow the entire circuitry to be fabricated from plastic. Although PMOS is preferably for the amorphous pixel driver transistors, external integrated circuit drivers fabricated on conventional silicon will generally employ NMOS transistors.

Referring now to FIG. 4, this shows an organic LED active matrix pixel driver circuit 400 which can be operated in a number of different modes, as described in UK patent application number 0126122.1.

As shown, the pixel driver circuit is provided with a ground (GND) line 402, a power or V_{ss} line 404, row select lines 406,

407 and a column data line 408. A reference current source (or sink) 424, preferably a programmable constant current generator, allows a current in column data line 408 to be adjusted to a desired level to set a pixel brightness. In other arrangements, however, a programmable voltage generator may be used additionally or alternatively to current generator 424, to allow the driver circuit to be used in other modes. Row driver circuitry 432 controls the first and second row select lines 406 and 407 according to the operating mode of the pixel driver circuitry.

The pixel driver circuit 400 comprises a driver transistor 410 connected in series with an organic LED display element 412 between the GND 402 and V_{ss} 404 lines. A storage capacitor 414, which may be integrated with the gate of transistor 410, stores a charge corresponding to a memorised gate voltage to control the drive current through OLED element 412.

Control circuitry for the pixel driver comprises two switching transistors 420, 422 with separate, independently controllable gate connections coupled to first and second select lines 406 and 407 respectively. A photodiode 416 is coupled to a node 417 between transistors 420 and 422. Transistor 420 provides a switched connection of node 417 to column data line 408. Transistor 422 provides a switched connection of node 417 to a node 415 to which is connected storage capacitor 414 and the gate of transistor 410. Again, preferably all the transistors of the pixel driver are PMOS.

As before a photodiode 416 is coupled between GND line 402 and line 417 so that it is reverse biased. The photodiode is physically arranged with respect to the OLED display element 412 to provide an optical feedback path 418, so that an illumination-dependent current flows in a reverse direction through photodiode 416, that is from GND line 402 towards V_{ss} .

When first select line 406 is active transistor 420 is on, that is the switch is "closed" and there is a relatively low impedance connection between column data line 408 and node 417. When first select line 406 is inactive transistor 420 is switched off and photodiode 416 is effectively isolated from column data line 408. When second select line 407 is active transistor 422 is switched on and nodes 415 and 417 are coupled; when second select line 407 is inactive transistor 422 is switched off and node 415 is effectively isolated from node 417.

It can be seen that when both transistors 420 and 422 are switched offside both the first and second select lines 406 and 407 are inactive) photodiode 416 is effectively isolated from the remainder of the driver circuitry. Similarly when transistor 422 is off (second select line 407 is inactive) and transistor 420 is on (first select line 406 is active) photodiode 416 is effectively connected between ground (GND) line 402 and column data line 408. In this way photodiode 416 may be effectively isolated from the remainder of the driver circuitry and used as a sensor.

The active matrix pixel driver circuitry 400 may be operated in a current-controlled mode with optical feedback, in a voltage-controlled mode with optical feedback, and in a voltage-controlled mode without optical feedback. Any or all of these modes may be employed with a light measurement mode to make an ambient light measurement before data is written to a pixel, or to input an image after data is written to a pixel.

The pixel driver circuit has a first mode of operation which, broadly speaking, is a previously described. In this mode first and second select lines 406 and 407 are connected together or driven in tandem by row drivers 432 so that the circuit operates as a current-controlled driver with optical feedback. As before, the programmable reference current generator 424

attempts to cause a reference current I_{col} to flow to off-pixel V_{ss} connection 426. Again off-pixel connection 426 may be connected to a drive voltage V_{drive} more negative than V_{ss} to permit a greater (more negative) drive to the gate of transistor 410.

In this first mode line 417 may be referred to as a current sense line, passing a current I_{sense} and line 415 may be referred to as a control line, passing a current I_{error} to set a voltage on capacitor 414 to control OLED 412. As before, when first and second (row) select lines 406 and 407 are active transistors 420 and 422 are on and $I_{col} = I_{sense} + I_{error}$ and thus the current I_{error} flows either onto or off capacitor 414 until OLED 412 illuminates photodiode 416 such that $I_{sense} = I_{col}$. At this point the first and second row select lines 406 and 407 can be deactivated and the voltage required for this level of brightness is memorised by capacitor 414.

In a second mode the pixel driver circuitry 400 is voltage controlled and operates in a similar manner to the prior art circuit of FIG. 1b, that is without optical feedback. As in the first mode of operation, the first and second select lines are connected together or driven in tandem by row drivers 432 but instead of column data line 408 being driven by a reference current generator 424, line 408 is driven by a voltage reference source, programmable to adjust the pixel brightness. The voltage source preferably has a low internal resistance to approximate a constant voltage source.

In this second mode of operation when the first and second select lines 406 and 407 are active capacitor 414 is coupled to column data line 408 and is therefore charged to the voltage output by the reference voltage generator. The small reverse current through photodiode 416 due to illumination by OLED 412 has a substantially no effect on the voltage on line 408 because of the low internal resistance of the voltage source. Once capacitor 414 has been charged to the required voltage transistors 420 and 422 are switched off by deasserting the first and second select lines 406 and 407, so that capacitor 414 does not discharge through photodiode 416. In this mode of operation the pair of transistors 420 and 422 effectively perform the same function as transistor 162 in the circuit of FIG. 1b.

In a third mode of operation the circuit is again driven by a programmable reference voltage source but the second select line is controlled so that it is always active (and hence so that transistor 422 is always on) whilst OLED 412 is on. In this way photodiode 416 is connected across storage capacitor 414 so that the circuit operates in substantially the same way as the circuit of FIG. 2b described above, transistor 420 performing the function of transistor 260 in FIG. 2b. In a simple embodiment the second select line 407 may simply be tied to a fixed voltage supply to ensure this line is always active. However transistor 422 need only be on long enough to ensure that capacitor 414 has enough time to discharge and thus it is still possible in this mode to switch off transistor 422 at times to allow photodiode 416 to be connected between lines 402 and 408 by transistor 420 and used as a sensor.

In an improvement of this mode of operation the programmable reference voltage source can be arranged to deliver a predetermined charge to capacitor 414 sine, when photodiode 416 is connected across capacitor 414, it is the charge on capacitor 414 which determines the apparent brightness of OLED 412 rather than the voltage itself. Delivering a predetermined charge to capacitor 414, rather than charging the capacitor to a reference voltage, reduces the effect of non-linearities in the charge-voltage characteristic of capacitor.

The pixel driver circuitry 400 may be controlled to provide a measurement cycle before pixel illumination data is written to the circuit to set the brightness of OLED 412. In the above

described modes it will be recognised that the first select line 406 in effect operates as a row select line whilst the second select line 407 operates as a combined mode and row select line. Thus, for example, in order to perform a (write black)—(measure)—(write level) cycle for a selected row the first select line 406 is held active whilst the second select line 407 is toggled from active during a write cycle to inactive or deasserted during a measure cycle.

FIG. 5 shows (not to scale) two alternative physical structures for OLED pixel driver circuits incorporating optical feedback FIG. 5a shows a bottom-emitting structure 500 and FIG. 5b shows a top-emitter 550.

In FIG. 5a an OLED structure 506 is deposited side-by-side with polysilicon pixel driver circuitry 504 on a glass substrate 502. The driver circuitry 504 incorporates a photodiode 508 to one side of the OLED structure 506. Light 510 is emitted through the bottom (anode) of the substrate.

FIG. 5b shows a cross section through an alternative structure 550 which emits light 560 from its top (cathode) surface. A glass substrate 552 supports a first layer 554 comprising the driver circuitry and including a photodiode 558. An OLED pixel structure 556 is then deposited over the driver circuitry 554. A passivation or stop layer may be included between layers 554 and 556. Where the pixel driver circuitry is fabricated using (crystalline) silicon rather than polysilicon or amorphous silicon a structure of the type shown in FIG. 5b is required and substrate 552 is a silicon substrate.

In the structures of FIGS. 5a and 5b the pixel driver circuitry may be fabricated by conventional means. The organic LEDs may be fabricated using either ink jet deposition techniques such as those described in EP 880303 to deposit polymer-based materials or evaporative deposition techniques to deposit small molecule materials. Thus, for example, so-called micro-displays with a structure of the type illustrated in FIG. 5b may be fabricated by ink jet printing OLED materials onto a conventional silicon substrate on which CMOS pixel driver circuitry has previously been fabricated.

With all these arrangements, however, it is generally desirable to reduce the power consumption of the active matrix display, and more particularly of the combination of the display and its (generally external) driver circuitry. It is flier desirable to reduce the maximum required power supply voltage for the display plus driver combination.

According to the present invention there is therefore provided a display driver for an electroluminescent display, the display comprising a plurality of electroluminescent display elements each associated with a display element driver circuit, each said display element driver circuit including a drive transistor having a control connection for driving the associated display element in accordance with a voltage on the control connection, the display driver comprising at least one display element brightness controller to provide an output to drive a said control connection to control the electroluminescent output from a said display element; a voltage sensor to sense the voltage on a said control connection; and a power controller for controlling an adjustable power supply for providing an adjustable voltage to said electroluminescent display to power said drive transistors for driving said display elements, said power controller being configured to provide a control signal to adjust said power supply voltage in response to said sensed voltage.

Sensing the voltage on a drive transistor control connection allows the strength of drive to be gauged and thus allows excess power dissipation in a drive transistor to be reduced by adjusting, and preferably reducing, the power supply accordingly. More particularly where the voltage on a control connection is less than the maximum available the voltage on the

control connection may be increased thus permitting a reduced voltage, power supply for the electroluminescent display elements and their associated driver transistors. The voltage on a said control connection will generally be sensed indirectly by sensing the voltage on a control line of the display, such as a column (or row) control line of an active matrix display. Depending upon the type of drive to the display, that is for example whether current or voltage drive is employed, an adjustment to the power supply voltage may bring about an automatic adjustment to the voltage on the drive transistor control connection.

In a preferred embodiment the drive transistor comprises a FET (or MOSFET) and the control connection comprises a gate connection of the transistor. Thus the voltage sensor senses the gate voltage of a drive transistor, and this may be accomplished by monitoring the voltage on a control line connection to the display. Even where the display element brightness controller provides a current rather than a voltage drive, sensing the voltage on a (current) control line nonetheless may, in effect, sense the gate voltage of a drive transistor. Thus the display driver may be employed with a conventional, unmodified active matrix display to increase the power efficiency of the display plus driver combination.

To optimise the efficiency of the display and driver combination it is preferable to use as small power supply voltage as possible. The required power supply voltage will, in part, be determined by the displayed image and hence by the data written to the display. More particularly the minimum usable power supply voltage will, in part, be determined by the power supply requirements of the brightest illuminated display element, and preferably the power supply voltage is no greater than required by this (or these) display element (or elements). However the minimum usable power supply voltage will also depend upon how hard the drive transistors may be driven on their control connections and, more particularly by the maximum drive available for the brightest illuminated pixel. It is therefore preferable to adjust the power supply until the control connection or gate voltage increases to the maximum available for driving the display and, as previously mentioned, this gate voltage may be monitored by monitoring a control line of the display. It will be appreciated that, generally speaking, reducing the power supply voltage will have the effect of increasing the control connection voltage since normally there is a mechanism for driving the display to produce a controlled brightness so that when the power supply voltage is reduced the control connection voltage is increased to compensate. This function may be performed by the display element brightness controller. An alternative way of picturing this mechanism is to consider it as control of the control connection or gate voltage to permit a reduction in the power supply voltage, although in practise this is less convenient to implement as a knowledge of the drive transistor characteristics may be required.

It will be appreciated that the brightness of a display element could be monitored, for example using a photodiode, to allow adjustment of the power supply voltage until the brightest illuminated element starts to get dimmer but it has been recognised that brightness information can, in effect, be derived more simply by monitoring a drive level, more particularly a drive transistor control connection voltage. It has also been recognised that this voltage may, in turn, be monitored by monitoring a brightness control connection to the display such as a current or voltage-controlled brightness setting line or connection.

In a preferred embodiment the display is an active matrix display with a plurality of row and column connections, for example, pixel select lines being connected to the row con-

nection and pixel brightness control lines being connected to the column connections. The voltage sensor may then, for example, sense the voltage on a brightness control or column connection.

In one embodiment the brightness controller comprises a substantially constant current generator, preferably adjustable to provide adjustable display element brightness. The constant current generator may comprise either a current source or a current sink. The voltage on a control connection of the display may then be substantially determined by a voltage level (input or output) of the constant current generator, which depends upon a current supplied by the generator. The power controller may then be configured to reduce the power supply voltage when the sensed voltage on a control connection is less in absolute terms (that is ignoring polarity) than a threshold voltage such as a maximum available voltage for driving the display. The sensed voltage for comparison with the threshold voltage preferably comprises a voltage sensed from a display element having a maximum brightness relative to others of the display elements at a given time, that is the brightest illuminated display element. It will be recognised that there may be more than one such pixel and that where the display is, for example, partitioned into sections with different drivers the maximum brightness of a display element in the appropriate partition for the driver may be employed.

In another embodiment the display element driver circuits are similar to the circuit described above with reference to FIG. 2b, that is voltage-controlled with a photo diode to provide optical feedback so that the voltage on the drive transistor control connection decays with time. In this embodiment the power controller may be configured to reduce the power supply voltage when the control connection voltage of the brightest illuminated display element has reduced to less than a first threshold value after a predetermined interval such as a line interval, frame interval or other cycle interval. The first threshold value may comprise, for example, a gate-source threshold voltage V_T of a FET or a base emitter voltage V_{be} of a bipolar transistor, or some other threshold value such as 0 volts. Broadly speaking the first threshold value is preferably selected to be substantially equal to a minimum control connection voltage required for the drive transistor to turn on. Preferably the power controller is configured to increase the power supply voltage when the control connection voltage has not decayed to less than a second threshold value, preferably equal to the first threshold value, after the predetermined interval.

Embodiments of the display driver may include the adjustable power supply.

In another aspect the invention provides a power controller for a display driver for an electroluminescent display, the display comprising a plurality of electroluminescent display elements each associated with a display element driver circuit, each said display element driver circuit including a drive transistor having a control connection for driving the associated display element in accordance with a voltage on the control connection, the power controller comprising a memory storing processor control code; a processor coupled to the memory for executing said processor control code; a sensed voltage input for sensing a voltage on a said control connection; and a control signal output for controlling an adjustable power supply for providing an adjustable voltage to said electroluminescent display to power said drive transistors for driving said display elements; said processor control code comprising instructions for controlling the proces-

sor to read said sensed voltage input and to output a control signal to adjust said power supply in response to said sensed voltage.

The invention also provides a carrier carrying the above-described processor-control code the carrier may comprise any conventional data carrier or storage medium such as a hard or floppy disk, ROM, or CD-ROM or an optical or electrical signal carrier.

In another related aspect the invention provides a method of operating an active matrix electroluminescent display, the display comprising a plurality of pixels each with an associated pixel driver, the display having a power supply and plurality of control lines for setting the brightness of each pixel, the method comprising setting the brightness pixels of the display using said control lines; monitoring control lines of the display, and reducing said power supply responsive to said monitoring.

The control lines may comprise, for example, column (or row) electrode lines of the display, although the skilled person will recognise that the active matrix display need not have pixels in a regular grid pattern. The display may be a colour display and the pixels may be of different colours or the pixels may all be of substantially the same colour, albeit preferably of variable brightness rather than merely on or off. The pixel brightness setting and control line monitoring may be combined.

The display pixels may include either a bipolar or FET (or MOSFET) driver transistor connected in series with an electroluminescent display element. The monitoring may thus monitor a control voltage of a pixel drive transistor, such as a base or gate voltage.

With a voltage-driven pixel driver the monitoring may determine whether the drive transistor control voltage is sufficient, or whether the power supply voltage is sufficient, by determining whether the brightest pixel is bright enough. This may be achieved by monitoring the control voltage of the drive transistor of the brightest illuminated pixel. Alternatively with a current drive in which, broadly speaking, the level of a substantially constant current generator sets the brightness of a pixel, the drive transistor control voltage may be monitored to determine whether or not the drive transistor could be driven harder, thus permitting the power supply voltage to be reduced. The monitoring may therefore comprise determining a maximum pixel brightness of the pixels which are illuminated (rather than, for example, a maximum possible pixel brightness) and the power supply may then be reduced to substantially no more than required by that maximum pixel brightness. Alternatively the power supply may be controlled so that it does not reduce the power supply voltage to less than required for the maximum required pixel brightness.

The minimum required power supply voltage depends upon the control voltage of the drive transistor for the brightest illuminated pixel. The power supply voltage may be set to the minimum required by reducing the power supply voltage until the control voltage of the drive transistor increases to the maximum available control voltage, that is the maximum control voltage which a display driver can provide to the display given the available power supply to the display driver. Thus the reducing may comprise reducing the power supply until the control voltage substantially reaches a maximum available control voltage, for instance a maximum voltage available at a control line of the display at the point of monitoring.

Where a voltage-driven display with optical feedback is employed such that the control voltage decays over time, the monitoring preferably monitors the decayed voltage, for

example after a predetermined time such as a frame interval where the voltage decays over a frame interval. The power supply voltage may be reduced if the control voltage, preferably of the brightest illuminated pixel, has decayed to less than a threshold voltage, and may otherwise be increased. In other words if the decayed voltage indicates that the pixel is sufficiently brightly illuminated the power supply voltage may be reduced until it is just sufficient (or just insufficient). As previously mentioned, the threshold voltage may comprise, for example, a threshold voltage of a FET driver transistor or a base emitter voltage of a bipolar driver transistor.

The invention also provides an active matrix display driver configured to operate in accordance with the above-described method. Thus the display driver may incorporate means for setting the brightness of pixels of the display, means for monitoring the control lines of the display, and means for reducing the power supply responsive to the monitoring.

In the above-described aspects of the invention the electroluminescent display is preferably an organic light emitting diode (OLED)-based display, such as a small molecule or polymer OLED-based display.

In all the above aspects of the invention the electro-optic or electroluminescent display element preferably comprises an organic light emitting diode.

These and other aspects of the invention will now be further described, by way of example only, with reference to the accompanying figures in which:

FIGS. 1a and 1b show, respectively, a basic organic LED structure, and a typical voltage-controlled OLED driver circuit;

FIGS. 2a and 2b show, respectively, a current-controlled OLED driver circuit, and a voltage-controlled OLED driver circuit with optical feedback according to the prior art;

FIGS. 3a to 3c show, respectively, a current-controlled OLED driver circuit with optical feedback, a first alternative switching arrangement, and a second alternative switching arrangement;

FIG. 4 shows a multimode organic LED driver circuit with optical feedback;

FIGS. 5a and 5b show vertical cross sections through device structures of OLED display elements with driver circuits incorporating optical feedback;

FIGS. 6a to 6c show, respectively, drain characteristics of an active matrix FET driver transistor, a graph of gate drive voltage against power supply voltage for constant drive current for an active matrix FET driver transistor, and a simplified active matrix pixel driver circuit;

FIGS. 7a and 7b show active matrix pixel brightness control-circuits;

FIG. 8 shows an active matrix display driver according to an embodiment of the present invention;

FIGS. 9a and 9b show, respectively, flow diagrams for power supply voltage control procedures for current- and voltage-controlled active matrix pixel driver circuits; and

FIG. 10 shows a circuit diagram of a maximum voltage detector and the display of the active matrix display driver of FIG. 8.

Referring now to FIG. 6a, this shows drain characteristics 600 for a FET driver transistor of an active matrix pixel driver circuit, such as transistors 212 and 256 of FIGS. 2a and 2b, transistor 310 of FIG. 3a and transistor 401 of FIG. 4. More particularly a set of curves 602, 604, 606, 608 is shown each illustrating the variation of drain current of the FET with drain-source voltage for a particular gate-source voltage. After an initial non-linear portion the curves become substantially flat, and the FET operates in the so-called saturation region. With increasing gate source voltage the saturation

drain current increases; below a threshold gate-source voltage V_T , the drain current is substantially 0. Typical values of V_T are between 1V and 6V. Broadly speaking the FET acts as a voltage controlled current limiter.

FIG. 6c shows a drive portion 640 of a typical active matrix pixel driver circuit. A PMOS driver FET 642 is connected in series with an organic light emitting diode 644 between a ground line 648 and a negative power line V_{ss} 646. FIG. 6b relates to the circuit of FIG. 6c and shows a graph 620 of gate-source voltage against V_{ss} , curve 622 illustrating the variation of V_{gs} with V_{ss} for a constant drain current, that is a constant current through OLED 644. Curve 622 comprises a substantially flat portion 624 corresponding to the flat portions of curves 602-608 and a non-linear portion 626. Dashed lines 628 and 630 correspond to a maximum available V_{gs} .

It will be appreciated from the circuit of FIG. 6c that, for a given OLED drive current, the greater V_{ss} the greater the excess (waste) power dissipation in driver transistor 642. It is therefore preferable to reduce V_{ss} as much as possible to reduce this excess dissipated power. However it can be appreciated from graph 620 that there is a limit, as indicated by dashed line 630, below which V_{ss} may not be reduced, this limit being determined by the maximum available V_{gs} and the required OLED drive voltage.

Still referring to FIG. 6b, as V_{ss} decreases initially V_{gs} changes little and, broadly speaking the operating point of driver transistor 642 moves along the flat portion of one of curves 602, 608 shown in FIG. 6a. However as V_{ss} continues to decrease V_{gs} must increase to maintain a constant I_d and hence a constant drive current through OLED 644. The driver circuit operates with optimum efficiency when V_{ss} is no greater than necessary, in other words when the supply voltage is not substantially greater than that needed to provide a desired OLED drive current when driver transistor 642 is driven with the maximum available drive voltage. The greater V_{ss} the greater I_d and hence the greater the OLED drive current although it will be recognised that there will come a point at which FET 642 no longer limits the drive current through OLED 64, instead the internal resistance of the OLED and other factors dominating to limit the current

Referring next to FIG. 7a, this shows a conceptual circuit diagram of a brightness control circuit 700 for the active matrix pixel driver 640 of FIG. 6c. A drive control circuit 702 is provided either for each pixel or for a column (or row) of the active matrix display. The drive control circuit 702 has a brightness control input 704 and a drive control output 708 driving the gate of transistor 642 with a voltage V_g . This gate voltage may be sensed by means of a connection 710 to drive control output 708; in a practical circuit connection 710 may be indirect, for example via one or more switching transistors. Drive control circuit 702 also has a drive sense input 706, for example to sense the drive current through OLED 644 either directly or indirectly, for example by sensing current through a photodiode optically coupled through OLED 644. Sensing arrangements have been previously been described with reference to FIGS. 2a, 3 and 4. The connection to drive sense input 706 is shown as a dashed line since although shown conceptually as tapping a point between transistor 642 and OLED 644 in practice the sensing arrangement generally includes intervening components, or may not comprise the physical connection shown.

FIG. 7b shows a more specific conceptual circuit 720 based on the arrangement of FIG. 7a. In FIG. 7b the function of drive control circuit 702 is performed by a current comparator 712, drive sense input 706 is a current drive sense input, and brightness control line 704 controls an adjustable constant current generator 714. Comparator 712 compares the sensed

drive current with the constant current from current (source or sink) generator 714 and provides a gate voltage output 708, for example to maintain the current sensed on input 706 substantially equal to the current set by constant current generator 714. In practice the current to voltage conversion may be implemented by a capacitor. As before a comparator 712 may be provided for each pixel or for a set of pixels, for example for each column of the display.

FIG. 8 shows a block diagram 800 of a display driver for an active matrix display 802, configured to control V_{ss} in accordance with the available active matrix pixel drive voltage to increase the power efficiency of the display plus driver combination.

In FIG. 8 the active matrix display 802 has a plurality of row electrodes 804a-e and a plurality of column electrodes 808a-e each connecting to internal respective row and column lines 806, 810 of which, for clarity, only two are shown. Power (V_{ss}) 812 and ground 818 connections are also provided, again connected to respective internal conducting traces 814 and 816 to provide power to the pixels of the display. For clarity a single pixel 820 is illustrated, connected as shown to V_{ss} , ground, row, and column lines 814, 816, 806, and 810. It will be recognised that in practice a plurality of such pixels is provided generally, but not necessarily, arranged in a rectangular grid and addressed by row and column electrodes 804, 808. The active matrix pixel 820 may comprise any conventional active matrix pixel driver circuit, such as the previously described circuits pixel driver circuits 200, 250, 300 and 400.

In operation each row of active matrix display 802 is selected in turn by appropriately driving row electrodes 804 and, for each row, the brightness of each pixel in a row is set by driving, preferably simultaneously, column electrodes 808 with brightness data. This brightness data as described above, may comprise either a current or a voltage. Once the brightnesses of the pixels in one row have been set the next row may be selected and the process repeated, the active matrix pixels including a memory element, generally a capacitor, to keep the row illuminated even when not selected. Once data has been written to the entire display, the display only needs to be updated with changes to the brightness of pixels.

Power to the display is provided by a battery 824 and a power supply unit 822 to provide a regulated V_{ss} output 828. Power supply 822 has a voltage control input 826 to control the voltage on output 828. Preferably power supply 822 is a switch mode power supply with rapid control of the output voltage 828, typically on a microsecond time scale where the power supply operates at a switching frequency 1 MHz or greater. Use of a switch mode power supply also facilitates use of a low battery voltage which can be stepped up to the required V_{ss} level, thus assisting compatibility with, for example low voltage consumer electronic devices.

The row select electrodes 804 are driven by row select drivers 830 in accordance with a control input 832. Likewise the column electrodes 808 are driven by column data drivers 834 in response to a data input 836. In the illustrated embodiment each column electrode is driven by an adjustable constant current generator 840, in turn controlled by a digital-to-analogue converter 838 coupled to input 836. For clarity only one such constant current generator is shown.

The constant current generator 840 has a current output 844 to source or sink a substantially constant current. The constant current generator 840 is connected to a power supply drive V_{drive} 842, which may be equal to (and connected to) V_{ss} but which is preferably greater than V_{ss} (in this example, more negative than V_{ss}) to allow active matrix pixel 820 to be driven harder than V_{ss} .

As the skilled person will appreciate, constant current generator **840** in effect adjusts the voltage on output **844** in order to attempt to maintain a substantially constant current in line **844**. Current generator **840** has a limit to the voltage it can provide which is termed (output voltage) compliance limit. The maximum constant current which can be supplied in line **844** is determined by the level of V_{drive} **842** and the compliance of the constant current generator. Any constant current generator may be employed, but a particularly advantageous form of constant current generator may be constructed using a bipolar transistor with its emitter and collector terminals directly connected to column line **844** and supply voltage V_{drive} **842**. This bipolar transistor may be incorporated into a current mirror, the output current being programmed or controlled by, for example, resistors switched using MOSFETs. Similar techniques are described in the applicant's co-pending UK patent application no. 0206062.2.

The voltage for V_{drive} may be provided, for example, by a separate output from power supply unit **822**.

The embodiment of the display driver illustrated in FIG. **8** shows a current-controlled active matrix display in which a column electrode current to set a pixel brightness. It will be appreciated that a voltage-controlled active matrix display, in which the brightness of a pixel is set by the voltage on a column line, could also be employed by using voltage rather than current drivers for column data drivers **834**.

The control input **832** of row select drivers **830** and the data input **836** of column data drivers **834** are both driven by display drive logic circuitry **846** which may, in some embodiments, comprise a microprocessor. The display drive logic **846** is clocked by a clock **848** and, in the illustrated embodiment, has access to a frame store **850**. Pixel brightness and/or colour data for display on display **802** is written to display drive logic **846** and/or frame store **850** by means of data bus **852**.

The display drive logic has a sense input **856** driven from the output of an analogue-to-digital converter **854**. Analogue-to-digital converter **854** is used to monitor the voltage on each of column electrodes **808a-e** that is, for example, the voltage on line **844**. To monitor these voltages a plurality of analogue-to-digital converters may be employed or one or more A/D converters may be time multiplexed to monitor the column electrode voltages. The voltages on the column electrodes correspond to the gate voltages of the pixel driver transistors in a selected row, as will be explained below for the specific examples of the previously described pixel driver circuits. Although not explicitly shown in FIG. **8** it is desirable, but not essential, also to measure the supply voltage V_{drive} **842**, for example for compliance determination. This may be done by using analogue-to-digital converter **854**, either by using a separate input on the converter or by time multiplexing the converter, or a separate analogue-to-digital converter may be employed to provide a V_{drive} sense signal to display drive logic **846**.

In FIG. **2a** when a row is selected transistors **220** and **222** are turned on and thus the column data line **210** is effectively connected to the gate of driver transistor **212**. In FIG. **3a** when row select line **306** is active transistors **320** and **322** are turned on and the gate of driver transistor **310** is effectively connected to column data line **308** and thus the voltage on column data line corresponds to the gate voltage of driver transistor **310**. In a similar way in FIG. **3b** transistor **350** connects column line **308** to driver transistor control line **315**, and in FIG. **3c** transistor **360** connects column line **308** to driver transistor control line **315**. In FIG. **4** column data line **408** is connected to the gate of driver transistor **410** when transistors **420** and **422** are on. It can therefore be appreciated that

although the aforementioned circuits employ a current to set the pixel brightness, the current in effect determines a gate voltage drive level to provide the required brightness and this gate voltage drive level appears on the relevant column data line. In the context of FIG. **8** it can be seen that this gate drive voltage will appear on the current output line **844** of constant current generator **40**. It will be appreciated that this is the case whether, as in circuit FIG. **2a**, the constant current generator sets the current in the driver transistor directly or whether, as for example in FIG. **3a**, the constant current generator sets a current in a photodiode, the driver transistor being driven such that the OLED brightness is that required by the photodiode current set by the constant current generator.

In the arrangement of FIG. **2b** when row conductor **262** is active transistor **260** is on and column conductor **264** is connected to the gate of the driver transistor **256**. Thus, again, the voltage on the column conductor **264** corresponds to that on the gate of the driver transistor **256**, although in the case of FIG. **2b**. It is the voltage on conductor **264** which determines the brightness of OLED **254**, as described above.

Referring again to FIG. **8**, the display drive logic **846** includes a gate voltage sense unit **858** and a power controller **860**. One or both of the sense unit and power controller may be implemented as processor control code where the display drive logic **846** includes a processor. The gate voltage sense unit **858** reads a voltage on sense input **856** and the power controller **860** outputs a voltage control signal to input **826** of power supply unit **822** to control power supply voltage V_{ss} in response to the sensed input voltage. The operation of the power controller is described in more detail below with reference to FIGS. **9a** and **9b** for current- and voltage-controlled active matrix displays respectively.

FIG. **9a** shows a flow diagram of a procedure which may be implemented by power controller **860** in embodiments of a display driver for driving a current-controlled active matrix display. Broadly speaking the power controller **860**, in conjunction with the gate voltage sense unit **858** and analogue-to-digital converter **854** scans all the pixels of display **802** to identify the brightest illuminated pixel, that is the pixel with the maximum drive transistor gate voltage, and then controls the power supply to reduce V_{ss} until the maximum gate voltage is substantially equal to the maximum voltage available given the level of V_{drive} **842** and the compliance of constant current generator **840**.

Referring to the flow chart, step **S900** the power controller **860** uses the gate voltage sensor **858** to read the gate voltage V_g for all the pixels by reading the voltage on column electrodes **808a-e** as each row of the display in turn is selected. The power controller then, at step **S902**, identifies the maximum V_g value of those read which, in effect, identifies the drive for the brightest pixel or pixels. In alternative embodiments the brightest pixel or pixels may be determined in some other way, for example by interrogating the data in frame store **850** or by tracking the data written to the display using bus **852**.

At step **S904** the power controller determines whether or not the maximum V_g is less than the maximum available V_g , that is in the circuit of FIG. **8** for example the maximum voltage which could be provided on a column drive line such as line **844**. If V_g is not less than the maximum available there is no scope to reduce the power supply voltage without reducing the brightness of the brightest illuminated pixel. More specifically, however, if V_g is not less than the maximum available drive voltage the power supply voltage V_{ss} is insufficient and is therefore increased, at step **S910**. The procedure then loops back to step **S900** to rescan the display so that changes in pixel brightness may be detected. If desired the V_g

thresholds for increasing and reducing V_{ss} may be different to provide a degree of hysteresis in the control of V_{ss} , for example making the threshold for reducing V_{ss} higher than that for increasing V_{ss} .

If, at step S904, it is determined that the drive voltage to the display is less than the maximum available drive voltage the power controller, at step S908, outputs a control signal to switch mode power supply unit 822 to reduce the power supply V_{ss} on line 828 to display 802. The procedure then again loops back to step S900 to re-check which pixel is most strongly driven and to recheck whether there is any further scope for reducing V_{ss} . The reduction in V_{ss} at step S908 may be small so that V_{ss} changes only gradually, which may be appropriate where the brightest pixel is, on average, not at maximum illumination or where the display is occasionally briefly black (that is non-illuminated). Alternatively the reduction in V_{ss} may be large where, for example, a rapid response is preferred.

As V_{ss} is reduced the constant current drive, that is the constant current generator 840 in the arrangement of FIG. 8, automatically increases the drive voltage to the display in order to attempt to drive the current required by the desired pixel brightness on to the relevant display control line. To read the drive voltage from the pixel or pixels with the maximum V_g the appropriate row of the display may be selected using row select drivers 830 and the voltage read using analogue-to-digital converter 854 whilst driving at least the monitored pixel (and, if necessary, all the pixels of the row to prevent loss of data) with its specified current drive using column data drivers 834.

FIG. 9b shows a flow chart for a similar procedure in which the active matrix display 802 is voltage driven, for example using pixel driver circuits similar to those shown in FIG. 2b. In FIG. 9b, as with FIG. 9a, the procedure initially, at step S920, reads the voltage drive for the pixels of the display and identifies the pixel with the maximum voltage drive. As described above, in the circuit of FIG. 2b the gate voltage of transistor 256 gradually decays according to the brightness of OLED 254. Thus, at step S922, the drive voltage of the pixel with the maximum gate voltage drive is monitored at the end of the relevant decay cycle, typically the end of a frame period. This function may be performed actively, for example by controlling row select drivers 830, but preferably is performed during the usual frame scanning process required by the circuit of FIG. 2b, for example by implementing a read-before-write data access cycle. Broadly speaking the procedure then checks to see whether the gate voltage has decayed sufficiently to switch off the OLED associated with the (brightest) pixel, that is in the context of FIG. 2b, to check whether photodiode 266 has substantially fully discharged gate capacitor 258. If the voltage has decayed sufficiently, that is if the gate capacitor is sufficiently discharged, the associated pixel OLED is sufficiently bright and the power supply voltage may be reduced, otherwise the power supply voltage may be increased. Thus V_{ss} is on/off servo controlled around the point of maximum efficiency operation for the display plus driver combination.

In more detail, at step S924 the drive voltage of the pixel with the greatest drive voltage is compared with a threshold voltage. This threshold voltage may be 0V, for example to check whether the gate capacitor has completely discharged, but is preferably a threshold gate voltage of the driver transistor as once the drive voltage falls below this threshold voltage the driver transistor will be switched off and the associated OLED non-illuminated. If the drive voltage is less than the threshold voltage the power supply voltage V_{ss} is more than required by the maximum brightness pixel and

thus, at step S926, V_{ss} is reduced and the procedure loops back to step 920. If the voltage has not decayed to the threshold voltage V_{ss} is insufficient for the maximum required pixel brightness and thus, at step S928, V_{ss} is increased and again the procedure looks back to step S920 to re-check all the pixels. If desired a degree of hysteresis may be incorporated into the V_{ss} control by making the threshold drive voltages for reducing and increasing V_{ss} different. More particularly the threshold or reducing V_{ss} may be lower (smaller in absolute terms) than the threshold for increasing V_{ss} .

In the procedures of FIG. 9a and/or FIG. 9b some or all of steps S908, S910, S926 and S928, in which the power supply voltage V_{ss} to the display is altered, may include an additional step of rewriting data to the display, in particular rewriting data setting the brightness of illuminated pixels of the display. The skilled person will recognise that changing the power supply to the display will have the effect of changing the brightness of the pixels to which data has already been written. This does not represent a significant problem in a voltage-controlled display employing pixels such as shown in FIG. 2b since such a display, in any case, is refreshed at regular intervals to compensate for the decay in the stored pixel voltages. However in a current-controlled display refresh of the display may only be carried out at longer intervals or, in some instances, not at all.

A small change in the overall brightness of the display may not be thought to represent a significant problem and whether or not elements of the display are refreshed may be determined based upon, for example, the magnitude of the changes to V_{ss} and the rapidity with which the displayed data is in any case changing. For example where the data is changing rapidly rewriting the displayed data may not be considered necessary. Alternatively the entire display may be scanned and rewritten at intervals although these intervals, need not correspond to the frame intervals conventionally associated with raster scanned or passive matrix displays as the purpose of the refresh is not to prevent flicker but merely to compensate for small brightness changes.

The procedures described with reference to FIGS. 9a and 9b lend themselves to digital implementation but the control functions may also be implemented in analogue circuitry or in a mixture of digital and analogue circuitry. In particular, FIG. 10 shows a circuit diagram of a maximum voltage detector which may be employed to determine the maximum value of V_g in step S902 of FIG. 9a or in step S920 of FIG. 9b.

In FIG. 10 each column electrode 808a-e is connected to a reactive diode 1002a-e to sample the voltage on each column line. The diode OR arrangement outputs on line 1004 the maximum voltage on any one of the column electrode lines less a diode voltage drop. A peak detect circuit 1005 comprises a capacitor 1006 to store the voltage on line 1004 and a controllable switch 1008 which is closed in response to a signal on reset line 1010 to reset the charge on capacitor 1006. The maximum detected voltage output on line 1004 may be buffered with a high input impedance amplifier. The reset line 1010 may be controlled by display drive logic 846 of FIG. 8 and the maximum column voltage output on line 1004 may be provided to an analogue digital converter, such as ADC 854 of FIG. 8, for digitisation prior to inputting to display drive logic 846. In this way the sensing circuitry and ADC 854 may be simplified.

Circuits and methods have been described with reference to their use for driving organic LEDs but the circuits and methods may also be employed with other types of active matrix electroluminescent display such as inorganic TFE (Thin Film Electroluminescent) displays, gallium arsenide on silicon displays, porous silicon displays, and the like. The

circuits and methods are not restricted to use with displays with pixel driver circuits of the types shown but may be employed with any display in which a current controls a display characteristic. Similarly applications of the invention are not limited to displays comprising a grid of pixels but may also be used with, for example, segmented displays.

No doubt many other effective alternatives will occur to the skilled person and it should be understood that the invention is not limited to the described embodiments.

The invention claimed is:

1. A display driver for an active matrix electroluminescent display, the display comprising a plurality of electroluminescent pixels each pixel comprising a pixel driver circuit and a display element, each said pixel driver circuit including a drive field effect transistor having a gate connection for driving the associated display element in accordance with a voltage on the gate connection to produce a driving current through said display element, the display driver comprising:

a display element brightness controller configured to provide an output to drive a said gate connection to control the electroluminescent output from a said pixel;

a voltage sensor to sense a said voltage on said gate connection; and

a power controller coupled to said voltage sensor for controlling an adjustable voltage power supply to each of said plurality of electroluminescent pixels, said power controller configured to read a sensed voltage on each said pixel gate connection within a predetermined period to identify a display element having a maximum brightness relative to others of said display elements within said predetermined period, wherein

said display element brightness controller and said power controller are configured to, respectively and concurrently within a period, increase said voltage on said gate connection of said pixel having said identified display element and to reduce said power supply voltage, to a point where the voltage of said adjustable voltage power supply is just sufficient to maintain a current to said identified display element substantially equal to a predetermined current corresponding to a current that is produced in said identified display element prior to said increasing of said voltage on said gate connection and said reducing of said power supply voltage, said increasing and said reducing in response to a said sensed voltage on said gate connection of said pixel having said identified display element, wherein said increasing and said reducing are performed as long as said sensed voltage on said gate connection is determined to be less than a maximum available voltage for outputting from said brightness controller to said display element and until said voltage on said gate connection substantially reaches said maximum available voltage.

2. A display driver as claimed in claim 1 wherein said voltage sensor is configured to sense the voltage on a said gate connection by sensing the voltage on an electrode of said display.

3. A display driver as claimed in claim 1 wherein a said pixel includes a photodiode, and wherein a photocurrent through said photodiode is determined by a said adjustable constant current to determine a brightness of said pixel.

4. A display driver as claimed in claim 1 wherein said power controller is further configured to increase said power supply voltage when said gate connection voltage of said brightest pixel has not reduced to less than a threshold value after a predetermined interval.

5. A display driver as claimed in claim 1 further comprising said adjustable voltage power supply.

6. A method of operating an active matrix electroluminescent display, the display comprising a plurality of electroluminescent pixels each pixel comprising an associated pixel driver and a display element, each said pixel driver including a drive field effect transistor having a gate connection for driving the associated display element in accordance with a voltage on the gate connection to produce a driving current through said display element, the display having an adjustable voltage power supply coupled to provide a power supply voltage to each of said plurality of electroluminescent pixels, and a plurality of control lines corresponding to said gate connections for setting the brightness of each pixel, the method comprising:

setting the brightness of pixels of the display using said control lines to drive said gate connections;

monitoring said control lines of the display to sense said voltages on said gate connections, and controlling said adjustable voltage power supply to each of said plurality of electroluminescent pixels by reading a sensed voltage on each said gate connection within a predetermined period to identify a display element having a maximum brightness relative to others of said display elements within said predetermined period; and

concurrently within a period, reducing said power supply voltage and increasing said voltage on said gate connection of said pixel having said identified display element, responsive to said monitoring to a point where a voltage of said adjustable voltage power supply is just sufficient to maintain a current to said identified display element substantially equal to a predetermined current corresponding to a current that is produced in said identified display element prior to said increasing of said voltage on said gate connection and said reducing of said power supply voltage, said increasing and said reducing in response to a said sensed voltage on said gate connection of said pixel having said identified display element, wherein said increasing and said reducing are performed as long as said sensed voltage on said gate connection is determined to be less than a maximum available voltage for outputting to said display element and until said voltage on said gate connection substantially reaches said maximum available voltage.

7. A method as claimed in claim 6 wherein a said pixel includes a photodiode and wherein a current through said photodiode is determined by an adjustable constant current.

8. An active matrix display driver configured to operate in accordance with the method of claim 6.

9. A display driver as claimed in claim 1 wherein said electroluminescent display comprises an organic light emitting diode display.

10. A method as claimed in claim 6 wherein said electroluminescent display comprises an organic light emitting diode display.

UNITED STATES PATENT AND TRADEMARK OFFICE
CERTIFICATE OF CORRECTION

PATENT NO. : 7,834,824 B2
APPLICATION NO. : 10/518182
DATED : November 16, 2010
INVENTOR(S) : Paul R. Routley et al.

Page 1 of 1

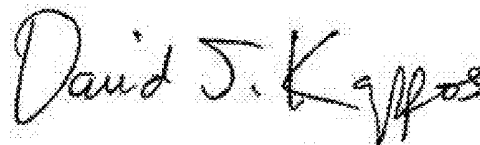
It is certified that error appears in the above-identified patent and that said Letters Patent is hereby corrected as shown below:

At Column 2, line 10, "activate&" should be -- activated --.

At Column 2, line 25, "it" should be -- it. --.

At Column 5, line 19, "photocurrent" should be -- photocurrent. --.

Signed and Sealed this
Thirty-first Day of May, 2011

A handwritten signature in black ink, reading "David J. Kappos". The signature is written in a cursive, flowing style with a large initial "D" and a stylized "K".

David J. Kappos
Director of the United States Patent and Trademark Office

专利名称(译)	显示驱动电路		
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申请号	US10/518182	申请日	2003-06-11
[标]申请(专利权)人(译)	劳特利PAUL - [R SMITH尤安Ç		
申请(专利权)人(译)	劳特利PAUL - [R SMITH尤安Ç		
当前申请(专利权)人(译)	剑桥显示科技有限公司		
[标]发明人	ROUTLEY PAUL R SMITH EUAN C		
发明人	ROUTLEY, PAUL R. SMITH, EUAN C.		
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CPC分类号	G09G3/3233 G09G3/325 G09G3/3291 G09G2300/0417 G09G2300/0819 G09G2300/0842 G09G2300/088 G09G2320/029 G09G2320/045 G09G2330/021 G09G2360/148		
优先权	2002013986 2002-06-18 GB		
其他公开文献	US20060038758A1		
外部链接	Espacenet USPTO		

摘要(译)

本公开一般涉及用于电光显示器的显示驱动器电路，并且更具体地涉及用于以更高效率驱动有源矩阵有机发光二极管显示器的电路和方法。一种用于电致发光显示器的显示驱动器，该显示器包括多个电致发光显示元件，每个电致发光显示元件与显示元件驱动电路相关联，每个显示元件驱动电路包括具有控制连接的驱动晶体管，用于根据电压驱动相关的显示元件在控制连接上，显示驱动器包括至少一个显示元件亮度控制器，以提供输出以驱动控制连接以控制来自显示元件的电致发光输出；电压传感器，用于检测控制连接上的电压；用于控制可调电源的电源控制器，用于向电致发光显示器提供可调电压，为所述驱动晶体管供电以驱动所述显示元件，所述电源控制器用于提供控制信号，以响应所述电源电压调节所述电源电压。感应电压。

